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Port Macquarie

Coffs Harbour

RGS01314.1-AB

11 July 2016

Stanwell Consulting 57 Irvine St BANKSTOWN NSW 2200

Delivered via email to: stanwellc@gmail.com

Attention: Sam Awad

Dear Sam.

RE: GEOTECHNICAL ASSESSMENT FOR PROPOSED TOWNHOUSE DEVELOPMENT 19 GREENVIEW CLOSE, FORSTER

1. INTRODUCTION

As requested, Regional Geotechnical Solutions Pty Ltd (RGS) has undertaken a geotechnical assessment for a proposed townhouse development at 19 Greenview Close, Forster (Lot 8 DP 806667). The provided drawings indicate that the proposed development involves the construction of five single and triple storey townhouses. The site is currently zoned R2 – Low Density Residential as per MidCoast Council's Local Environment Plan.

The purpose of the assessment was to provide an appraisal of the geotechnical conditions at the site to allow for the design of foundations and to assess for the presence of Acid Sulfate Soils (ASS) in the southern half of the site. It has been assumed that the structure will meet the performance expectations set out in AS2870-2011.

2. METHODOLOGY

Field work involved a general site walkover, observation of the site conditions, and the drilling of five boreholes (BH1 to BH5) within the proposed building footprint and stormwater drainage retention area. The subsurface profile encountered in the boreholes is presented on the attached Engineering Logs. The borehole locations are presented on Figure 1. Two laboratory Shrink-Swell tests were undertaken on representative samples of the clay encountered.



3. SITE CONDITIONS

The property occupies 1,810m², is irregular in shape and bound by Greenview Close to the north, existing residential properties to the east and west and by Tea Tree Road to the south.

The site is located in an area of gently to moderately undulating terrain and is situated toward the top of a north to south trending slope. The front portion of the site slopes toward the south and south west in the order of $1^{\circ} - 3^{\circ}$. The back (southern) portion of the site slopes to the south and south west in the order of $3^{\circ} - 5^{\circ}$. The proposed building site is comprised of thick grass and weeds. Pipers Bay is located approximately 180m to the south west of the site.

Drainage of the site is likely to be from a combination of surface infiltration and overland runoff into the Greenview Place street drainage system. At the time of the field work, the proposed building area was vacant.

Images of the site are provided below.



Location of 19 Greenview CI, Forster





Looking south west over site from Greenview Cl.



Looking north over site from the rear of the property.



Looking south west over site showing the rear property boundary.



Looking north east over site toward Greenview CI.

Reference to the 1:100,000 Bulahdelah Geology Map 9333 shows the property to be within an area underlain by the Bundook Beds that contain grey to brown lithic sandstone and siltstone, which is frequently cherty and ribbon banded, interbedded with massive greywackes and minor conglomerate and limestone.

The boreholes drilled within the proposed building area and stormwater drainage retention area encountered up to 0.3m of topsoil/fill, underlain by up to 0.55m of alluvium, underlain by extremely weathered siltstone to at least 1.6m depth.

Groundwater was not encountered in the boreholes. Groundwater levels fluctuate as a result of seasonal variations, temperature, rainfall and other similar factors, the influence of which may not have been apparent at the time of the assessment.



4. SITE CLASSIFICATION

Laboratory testing on two representative samples of alluvial clay from BH2 and BH5 indicated that the natural material at the site has a shrink-swell index of between 3.5% and 4.7%.

On the basis of the conditions encountered in the undisturbed natural ground and the laboratory test results, the site is classified as **Class 'M'** (Moderately Reactive) in accordance with AS2870-2011. Structural footings that are extended to found within the underlying very stiff natural alluvial clay and weathered siltstone can be designed based on a **Class 'M'** classification with a characteristic free surface movement of 40mm and an allowable bearing pressure of 100kPa. Footings and slabs can be designed on the basis of AS2870-2011 recommendations for a Class M site.

Where structures are founded partially within weathered rock and partially on clay soils, differential shrink-swell related movements can be accommodated either by provision of articulation or by placing all foundations within highly weathered rock.

Fill that is not placed and compacted as Controlled Fill should not be used for the support of high level footings. In such areas, footings should be deepened to extend through the fill to the underlying weathered rock. Footings placed on weathered rock in this manner can be designed on the basis of a maximum allowable end bearing pressure of 300kPa. All footings are to be founded outside or below all zones of influence resulting from existing or future service trenches.

Of particular importance will be the planting of future trees and shrubs that may affect the moisture profile in the vicinity of the footings. Potential surface movements must take into account the potential swelling effects resulting from the removal of the trees which have been calculated in accordance with the methodology outlined in AS2870-2011 (Appendix H).

Any foundations located within areas where tree removal has previously been carried out will need to be taken through the disturbed ground to be founded on the undisturbed natural ground beneath. All organic root material should be removed from within the building footprint.

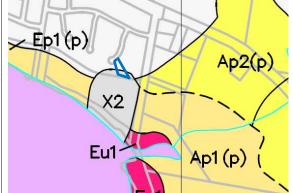
Footings should not be founded within topsoil or within fill.

5. ACID SULFATE SOILS

Reference to the Forster 1:25,000 Acid Sulfate Soil (ASS) Risk Map indicates that the northern half of the site is an area of where there is No Known Occurrence of ASS. The risk map also indicates that the southern half of the site is comprised of Disturbed Terrain. Soil investigations are required to assess areas of disturbed terrain for ASS potential.







Location of site in red as indicated by Google Earth image

Extract from Forster 1:25,000 ASS Risk Map indicates the site (shown in blue) to be an area of high probability of occurrence of ASS.

Acid Sulfate Soils (ASS) produce sulphuric acid when exposed to oxygen due to the presence of iron sulphides in the form of pyrite within the soil matrix. These soils form when iron-rich sediments are deposited in saltwater or brackish water environments. Prior to oxidation, these pyritic soils are referred to as Potential ASS. ASS that have produced acid as a result of oxidation are referred to as Actual ASS. They typically occur in natural, low-lying coastal depositional environments below approximately 5m AHD. In the field, ASS are generally identified as saline sediments such as alluvial or estuarine soils or bottom sediments in creeks and estuaries.

Laboratory testing of representative samples collected from boreholes BH1, BH3 and BH4 was undertaken. Test locations are shown on Figure 1.

Three samples obtained were screened for the presence of actual or potential ASS using methods 23Af and 22Bf of the ASSMAC Acid Sulfate Soils Manual. The test results are attached. The results indicated:

- The samples revealed pH_f values of 5.00 to 5.55 in distilled water. In this test, pH <4 is an
 indicator of Actual ASS;
- The samples revealed pH_{FOX} values of 2.64, 2.98 and 3.26 in hydrogen peroxide. Values of less than 3 can be an indicator of Potential ASS.

To provide a more comprehensive assessment, the samples were submitted for Chromium Reducible Sulphur (CRS) analysis. A summary of the test results are presented in Table 1.



Table 1: Summary of ASS CRS Test Results

Davahala	Depth	Tavdova	Acid Trail	Sulfur Trail (% S Oxidisable)				
Borehole	(m)	Texture	TAA	Action Criteria	S _{kcl}	Scr	Action Criteria	
BH1	0.5 – 0.7	Fine	43	18	0.004	0.005	0.03	
вн3	0.2 – 0.5	Fine	67	18	0.004	0.010	0.03	
BH4	0.3 – 0.5	Fine	104	18	0.003	0.010	0.03	

Note: *

Testing undertaken on the coarse fraction of material retained on 75 □ m sieve

A review of the above results indicates the following:

- Each of the samples recorded a Titratable Actual Acidity (TAA) above the adopted action criteria indicating the presence of actual acidity;
- Oxidisable sulfur (S_{cr}) results were below the adopted action criteria in each of the samples which indicates the acidity is not sulphuric in nature.

Based on the results, the soils encountered within the assessment are acidic in nature but are not considered to be Acid Sulfate Soils due to the absence of oxidisable sulfur. As such, an Acid Sulfate Soil Management Plan will not be required. However, it would be prudent to apply lime at a rate of 8kg/tonne (dry weight) to excavation spoil that is to be re-used in order to neutralise the acid which is present in the site soils. It is recommended that good quality agricultural lime be used and thoroughly mixed through before re-use.

6. LIMITATIONS

The subsurface information collected is specific to borehole locations only. Although efforts have been made to distribute boreholes to give a good spatial coverage of the site it is unlikely the information is indicative of the full range of conditions which may be encountered during construction. If conditions other than those described in this report are encountered during construction, further advice should be sought without delay. Shrink-swell related movements can be affected by alterations to the soil profile by cutting and filling, and by the suction related effects of trees close to the building area. The effects of any such cutting, filling, tree planting should be taken into account when selecting design values for differential movement across the building. It is recommended that all foundations be founded on similar materials to reduce the potential for differential movement.

This site classification is provided on the basis that the performance expectations set out in AS2870-2011 will be acceptable for the proposed structure.

Please do not hesitate to contact the undersigned if you have any questions regarding this or any other project, or require any additional consultations.



For and on behalf of

Regional Geotechnical Solutions Pty Ltd

Andrew Hills

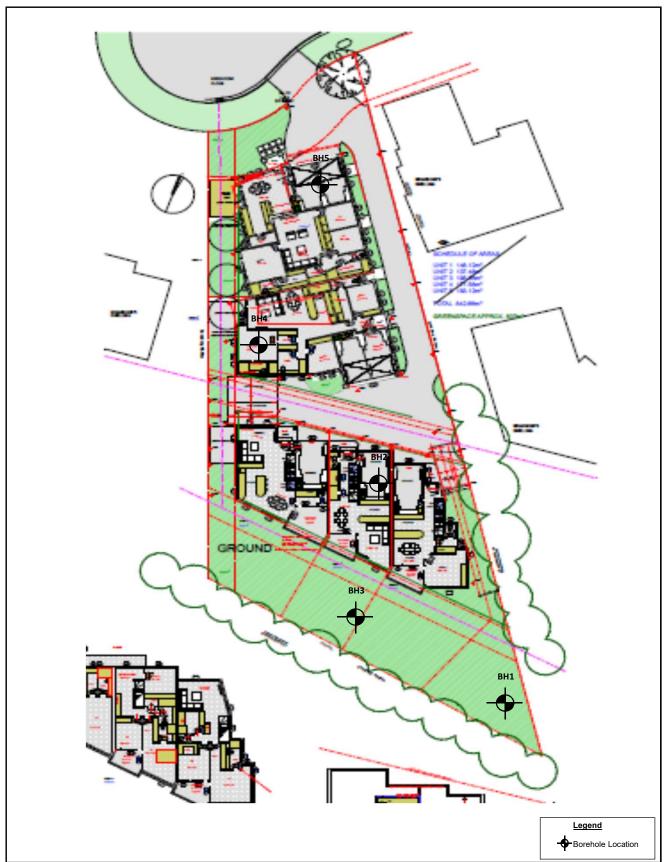
Environmental Engineer

Andre My

Attached: Figure 1 – Borehole Location Plan

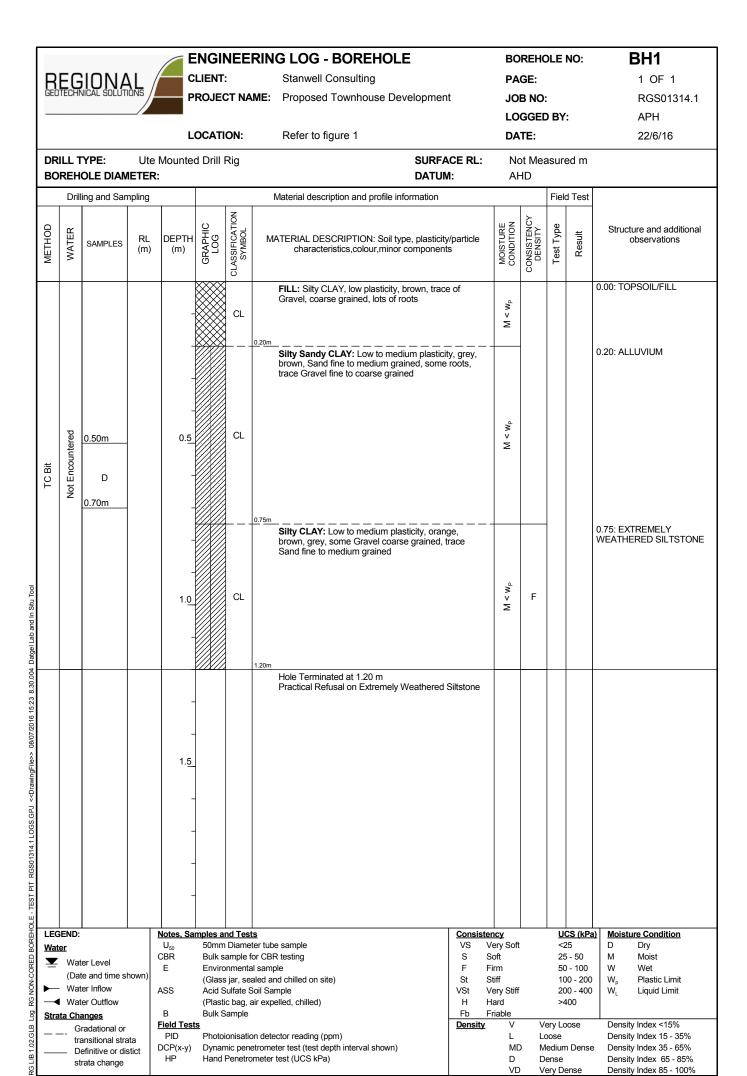
Engineering Logs

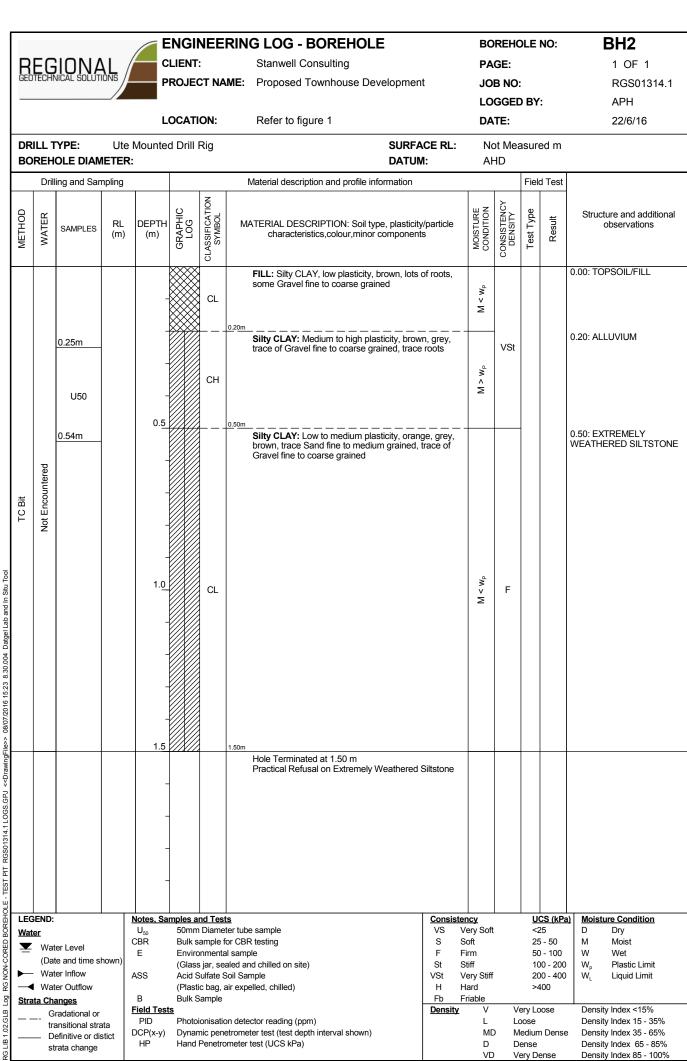
Laboratory Test Results



REGIONAL GEOTECHNICAL SOLUTIONS	F
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Client	Stanwell Consulting	Job No.	RGS01314.1
Project:	Proposed Townhouse Development	Drawn By:	APH
	19 Greenview Close, Forster	Date:	8-Jul-16
Title:	Borehole Location Plan	Drawing No.	Figure 1





nterval shown)

ı		
	LEG	END:
	Wate	<u>er</u>
I	\blacksquare	Water Level
I		(Date and time shown
ı	—	Water Inflow
ı	-	Water Outflow
ı	Stra	ta Changes
ı		Gradational or
ı		transitional strata
ı	_	 Definitive or distict
		strata change
•		

Notes, Sa	mples an	d Test	ts_	
U ₅₀	50mm [Diame	eter tube sample	
CBR	Bulk sa	mple f	for CBR testing	
E	Environ	menta	al sample	
			ealed and chilled on si	te)
ASS	Acid Su	Ilfate S	Soil Sample	
	(Plastic	bag, a	air expelled, chilled)	
В	Bulk Sa	mple		
Field Teet				

	(Glass jai, scaled and chilled on site)
ASS	Acid Sulfate Soil Sample
	(Plastic bag, air expelled, chilled)
В	Bulk Sample
Field Tests	<u>i</u>
PID	Photoionisation detector reading (ppm)
DCP(x-y)	Dynamic penetrometer test (test depth in
HP	Hand Penetrometer test (UCS kPa)

Consi	sten	cy		UCS (kPa)		1)	Moisture Condition			
VS	Ve	ery Soft		<2	25		D	Dry		
S	Sc	oft		25	5 - 50		M	Moist		
F	Fir	rm		50	- 100		W	Wet		
St	St	iff		10	0 - 200		W_p	Plastic Limit		
VSt	Ve	ery Stiff		20	0 - 400		WL	Liquid Limit		
Н	Ha	ard		>4	100					
Fb	Fr	iable								
Density		V	V	ery Lo	ose		Density Index <15%			
		L	Lo	ose			Dens	sity Index 15 - 35%		

Medium Dense

Dense

Very Dense

Density Index 35 - 65%

Density Index 65 - 85%

Density Index 85 - 100%

MD

D

VD



ENGINEERING LOG - BOREHOLE

Stanwell Consulting

PROJECT NAME: Proposed Townhouse Development

JOB NO:

PAGE:

BOREHOLE NO:

1 OF 1 RGS01314.1

BH3

LOGGED BY: APH

LOCATION: Refer to figure 1							DA	DATE:			22/6/16		
	DRILL TYPE: Ute Mounted Drill Rig SURFACE RL: BOREHOLE DIAMETER: DATUM:									Not Measured m AHD			
	Dril	ling and San	npling				Material description and profile information				Field	d Test	
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity characteristics,colour,minor components		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations
		0.20m		-		CL	FILL: Sitty CLAY, low plasticity, brown, lots of some Gravel fine to coarse grained	of roots,	M < W _P				0.00: TOPSOIL/FILL
Bit	Not Encountered	D 0.50m		- 0.5		CL	Silty Sandy CLAY: Low to medium grained fine to medium grained, some roots, trace G fine to coarse grained		M < w _P	St			0.20: ALLUVIUM
TC Bit	Not En	0.3011		- - - 1.0		CL	Silty CLAY: Low to medium plasticity, orang brown, trace of Sand fine to medium grained Gravel fine to coarse grained	ge, grey, d, trace	M < w _P	F			0.50: EXTREMELY WEATHERED SILTSTONE
LEC War				- 1. <u>5</u> -			Hole Terminated at 1.00 m						
LEC Wat	✓ War (Da – War ■ War ata Ch — G tr.	ter Level te and time she inflow ter Outflow anges radational or ansitional stra efinitive or dis rata change	nown)	Notes, Sa U ₅₀ CBR E ASS B Field Test PID DCP(x-y) HP	50mm Bulk s Enviro (Glass Acid S (Plast Bulk S S Photo Dynar	n Diame cample f conmenta s jar, se Sulfate S ic bag, a Sample ionisationic pene	ser tube sample or CBR testing I sample alled and chilled on site) ioil Sample air expelled, chilled) on detector reading (ppm) etrometer test (test depth interval shown) meter test (UCS kPa)	S S F F St S VSt V H F	ncy /ery Soft Soft Firm Stiff /ery Stiff Hard Friable V L MD D	Lo M D	<2 25 50 10 20 >4 ery Lo	6 - 50 0 - 100 00 - 200 00 - 400 000 00se	D Dry M Moist W Wet W _p Plastic Limit U _L Liquid Limit Density Index <15% Density Index 15 - 35%



ENGINEERING LOG - BOREHOLE

Stanwell Consulting

PROJECT NAME: Proposed Townhouse Development

JOB NO:

BOREHOLE NO:

LOGGED BY:

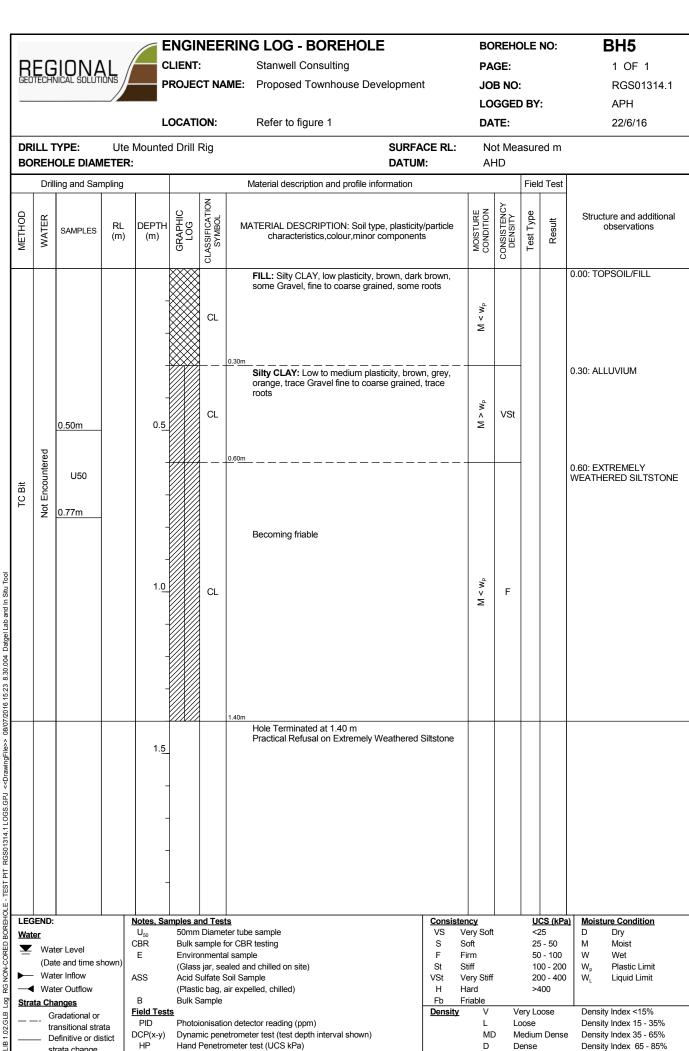
PAGE:

1 OF 1 RGS01314.1 APH

BH4

LOCATION: Refer to figure 1 **DATE:** 22/6/16

				L	OCAT	ON:	Refer to figure 1		DA	TE:			22/6/16	
DRILL TYPE: Ute Mounted Drill Rig BOREHOLE DIAMETER:						Rig SURFACE RL: DATUM:				Not Measured m AHD				
Drilling and Sampling							Material description and profile information				Field	d Test		
METHOD	WATER	SAMPLES	RL (m)	DEPTH (m)	GRAPHIC LOG	CLASSIFICATION SYMBOL	MATERIAL DESCRIPTION: Soil type, plasticity characteristics, colour, minor component		MOISTURE	CONSISTENCY DENSITY	Test Type	Result	Structure and additional observations	
					-		CL	FILL: Silty CLAY, low plasticity, brown, dark some Gravel fine to coarse grained, some		M × M				0.00: TOPSOIL/FILL
TC Bit		0.30m D 0.50m		- 0. <u>5</u>		CL	Silty CLAY: Low to medium plasticity, grey orange, some Gravel fine to coarse grained roots Becoming pale grey/pale brown/orange Becoming medium to high plasticity			VSt			0.20: ALLUVIUM	
	Not Encountered	0.50m		1.0_		CL	Silty CLAY: Low to medium plasticity, pale grey, pale brown, orange, trace Sand fine to medium grained, trace Gravel fine to medium grained. Becoming friable		M > W _P	St-F			0.60: EXTREMELY WEATHERED SILTSTONE	
				-			Hole Terminated at 1.60 m Practical Refusal on Extremely Weathered	Siltstone						
Wat	Wai (Da - Wai Wai ata Ch G tri	ter Level te and time she ter Inflow ter Outflow anges radational or ansitional strat efinitive or dist rata change	own)	Notes, Sa U ₅₀ CBR E ASS B Field Test PID DCP(x-y) HP	50mm Bulk s Enviro (Glass Acid s (Plast Bulk s s Photo Dynar	n Diamei sample fi ponmenta s jar, sea Sulfate S ic bag, a Sample ionisatio mic pene	ser tube sample or CBR testing I sample alled and chilled on site) ioil Sample sir expelled, chilled) on detector reading (ppm) etrometer test (test depth interval shown) meter test (UCS kPa)	S S F F St S VSt V	Pency Very Soft Soft Firm Stiff Very Stiff Hard Friable V L ME D VD	V Lc) M	<2 25 50 10 20 >4 ery Lo	6 - 50 0 - 100 10 - 200 10 - 400 100 100se	D Dry M Moist W Wet W _p Plastic Limit W _L Liquid Limit Density Index <15% Density Index 15 - 35%	



E-T				
RG LIB 1.02.GLB Log RG NON-CORED BOREHOLE - T	LEG	END:		
BOR	Wat	<u>er</u>		
RED	_	Wat	er Level	
20-		(Dat	e and time s	hown
ő	—	Wat	er Inflow	
RG	-	Wat	er Outflow	
Log	Stra	ta Cha	anges	
SLB		G	radational or	
02.0			ansitional stra	
IB 1.			efinitive or dis	stict
RG L		st	rata change	

Notes, Sam	ples and Tests
U ₅₀	50mm Diameter tube sample
CBR	Bulk sample for CBR testing
E	Environmental sample
	(Glass jar, sealed and chilled on site)
ASS	Acid Sulfate Soil Sample
	(Plastic bag, air expelled, chilled)
В	Bulk Sample
Field Tests	

В	Bulk Sample
Field Tests	
PID	Photoionisation detector reading (ppm)
DCP(x-y)	Dynamic penetrometer test (test depth interval shown)
HP	Hand Penetrometer test (UCS kPa)

Consi	<u>stency</u>	UCS (kPa)	Moisture Condition					
VS	Very Soft	<25	D	Dry				
S	Soft	25 - 50	M	Moist				
F	Firm	50 - 100	W	Wet				
St	Stiff	100 - 200	W _p	Plastic Limit				
VSt	Very Stiff	200 - 400	WL	Liquid Limit				
Н	Hard	>400						
Fb	Friable							
Densit	t y V	Very Loose	Density Index <15%					
	L	Loose	Density Index 15 - 35%					

Medium Dense

Very Der

Density Index 35 - 65%

Density Index 65 - 85%

Density Index 85 - 100%

MD

D

VD



02 4968 4468 02 4960 9775

E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896



Shrink Swell Index Report

Regional Geotechnical Solutions Pty Ltd

44 Bent Street

Wingham NSW 2429

Principal:

Project No.: MNC16P-0001 Project Name: Various Testing

Report No: SSI:NEW16W-1654--S01 Issue No: 1



Client Sample ID:

Sampling Method:

Date Sampled:

Date Submitted:

Shrink Test

Accredited for compliance with ISO/IEC 17025 The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

Approved Signatory: Dane Cullen

(Senior Geotechnician) NATA Accredited Laboratory Number: 18686 Date of Issue: 5/07/2016

Sample Details

Sample ID: NEW16W-1654--S01

Test Request No.: RGS01314.1

Material: Clay

Source: On-Site Insitu

Specification: No Specification

Project Location: 19 Greenview Close, Forster, NSW

BH2 - (0.25 - 0.54m) Sample Location:

Borehole Number:

Borehole Depth (m): 0.25 - 0.54m

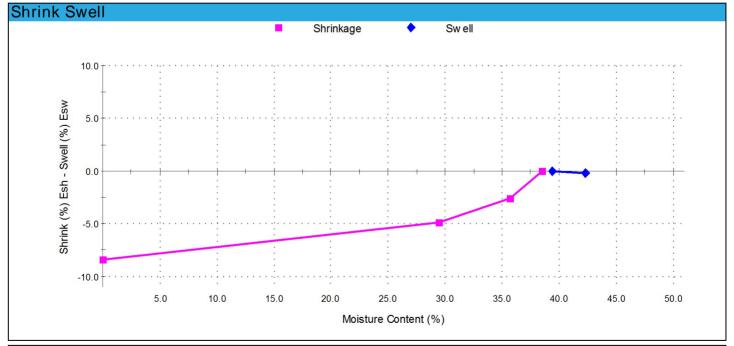
AS 1289.7.1.1

Sampled by Client 23/06/2016

24/06/2016

Shrink on drying (%): 8.4 Shrinkage Moisture Content (%): 38.5 Est. inert material (%): Crumbling during shrinkage: Cracking during shrinkage: Major

AS 1289.7.1.1 Swell Test Swell on Saturation (%): -0.2 39.4 Moisture Content before (%): 42.3 Moisture Content after (%): Est. Unc. Comp. Strength before (kPa): 600 Est. Unc. Comp. Strength after (kPa):



Shrink Swell Index - Iss (%): 4.7

Comments



02 4968 4468 02 4960 9775

E: admin@qualtest.com.au W: www.qualtest.com.au ABN: 98 153 268 896



Shrink Swell Index Report

Regional Geotechnical Solutions Pty Ltd

44 Bent Street

Wingham NSW 2429

Principal:

Project No.: MNC16P-0001 Project Name: Various Testing

Report No: SSI:NEW16W-1654--S02 Issue No: 1



Client Sample ID:

Sampling Method:

Date Sampled:

Date Submitted:

Accredited for compliance with ISO/IEC 17025 The results of the tests, calibrations and/or measurements included in this document are traceable to Australian/national standards

Approved Signatory: Dane Cullen

(Senior Geotechnician) NATA Accredited Laboratory Number: 18686 Date of Issue: 5/07/2016

Sampled by Client 23/06/2016

24/06/2016

Sample Details

Sample ID: NEW16W-1654--S02

Test Request No.: RGS01314.1

Material: Clay

Source: On-Site Insitu

Specification: No Specification

Project Location: 19 Greenview Close, Forster, NSW

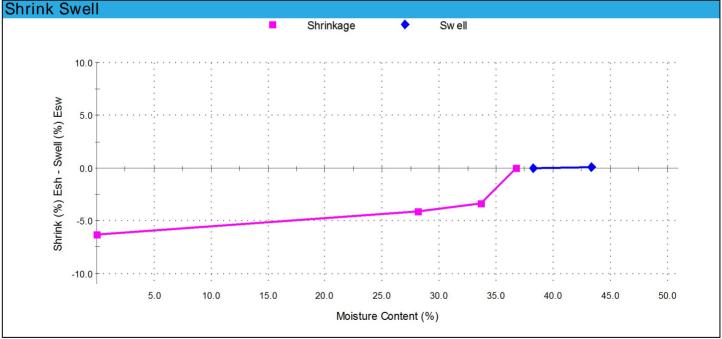
BH5 - (0.50 - 0.77m) Sample Location:

Borehole Number: Borehole Depth (m): 0.5 - 0.77m

> AS 1289.7.1.1 Shrink Test

Shrink on drying (%): 6.3 Shrinkage Moisture Content (%): 36.7 Est. inert material (%): Crumbling during shrinkage: Cracking during shrinkage: Major

AS 1289.7.1.1 Swell Test Swell on Saturation (%): 0.1 38.2 Moisture Content before (%): Moisture Content after (%): 43.3 Est. Unc. Comp. Strength before (kPa): 600 Est. Unc. Comp. Strength after (kPa):



Shrink Swell Index - Iss (%): 3.5

Comments

RESULTS OF ACID SULFATE SOIL ANALYSIS

3 samples supplied by Regional Geotechnical Solutions Pty Ltd on 24th June, 2016 - Lab. Job No. F1279 Analysis requested by Andrew Hills. **Your Project: RGS01314.1**

(44 Bent Street WINGHAM	NSW 2429)														Required if pr	1 _{KCL} <4.5		
Sample Site	EAL	TEXTURE	MOISTURE		FIELD/ LAB PEROXIDE SCREENING TECHNIQUE			TITRATABLE ACTUAL ACIDITY (TAA)		Extractable Extractable sulfate sulfur	REDUCED INORGANIC SULFUR		RETAINED ACIDITY (HCL extract) S _{NAS}		NET ACIDITY Chromium Suite	LIME CALCULATION Chromium Suite		
	code				Initial pH _F	pH _{FOX}				(To pH 6.5)	%S _{kcl}	(equivalent mole H+/tonne)		mium reducible S)	(as %S _{HCL} - %S _{kcl})		mole H ⁺ /tonne	kg CaCO ₃ /tonne DW
		(note 7)	(% moisture			peroxide	pH change	Reaction										(includes 1.5 safety Factor
			of total wet weight)	dry soil)					pH _{KCI}	(mole H ⁺ /tonne)			(%Scr)	(mole H ⁺ /tonne)	(%S _{NAS})	(mole H*/tonne)	(based on %Scrs)	when liming rate is [†] ve)
Method Info.		**		rx					(ACTUAL	ACIDITY-Method 23)			(POTENTIAL	ACIDITY-Method 22B)	(RETAINED A	ACIDITY)	** & note 5	** & note 4 and 6
BH1 0.5-0.7 BH3 0.2-0.5	F1279/1 F1279/2	Fine Fine	16.9 20.0	0.20 0.25	5.55 5.29	2.98 2.64	-2.57 -2.65	Medium High	4.43 4.18	43 67	0.004 0.004	2	0.005 0.010	3	0.005 0.008	2	49 76	4
BH4 0.3-0.5	F1279/3	Fine	26.6	0.23	5.00	3.26	-1.74	Medium	4.16	104	0.004	2	0.010	6	0.006	3	113	8

NOTE:

- 1 All analysis is Dry Weight (DW) samples dried and ground immediately upon arrival (unless supplied dried and ground)
- 2 Samples analysed by SPOCAS method 23 (ie Suspension Peroxide Oxidation Combined Acidity & sulfate) and 'Chromium Reducible Sulfur' technique (Scr Method 22B)
- 3 Methods from Ahern, CR, McElnea AE , Sullivan LA (2004). Acid Sulfate Soils Laboratory Methods Guidelines. QLD DNRME.
- 4 Bulk Density is required for liming rate calculations per soil volume. Lab. Bulk Density is no longer applicable field bulk density rings can be used and dried/weighed in the laboratory.
- 5 ABA Equation: Net Acidity = Potential Sulfidic Acidity (le. Scrs or Sox) + Actual Acidity + Retained Acidity measured ANC/FF (with FF currently defaulted to 1.5) 6 The neutralising requirement, lime calculation, includes a 1.5 safety margin for acid neutralisation (an increased safety factor may be required in some cases)
- 6 The neutralising requirement, time calculation, includes a 1.5 safety margin for acid neutralisation (an increased safety factor may be required in some case
 7 For Texture: coarse = sands to loamy sands; medium = sandy loams to light clays; fine = medium to heavy clays and silty clays
- 8 .. denotes not requested or required. '0' is used for ANC and Snag calcs if TAA pH <6.5 or >4.5
- 9 SCREENING, CRS, TAA and ANC are NATA accredited but other SPOCAS segments are currently not NATA accredited
- 10- Results at or below detection limits are replaced with '0' for calculation purposes.
- 11 Projects that disturb >1000 tonnes of soil, the ≥0.03% S classification guideline would apply (refer to acid sulfate management guidelines).
- 12 Results refer to samples as received at the laboratory. This report is not to be reproduced except in full.
- 13 ** denotes these test procedure or calculation are as yet not NATA accredited but quality control data is available

(Classification of potential acid sulfate material if: coarse Scr≥0.03%S or 19mole H*/t; medium Scr≥0.06%S or 37mole H*/t; fine Scr≥0.1%S or 62mole H*/t) - as per QUASSIT Guidelines



Required if pU 44 E

checked: Graham Lancaster Laboratory Manager