STUDENT MANUAL FOR

# THE FELECTRONICS

THOMAS C. HAYES PAUL HOROWITZ

# Class 1: DC Circuits

#### Topics:

- What this course treats: <u>Art?</u> of Electronics DC circuits
   Today we will look at circuits made up entirely of
  - DC voltage sources (things whose output voltage is constant over time; things like a battery, or a lab power supply);
     and
  - resistors.

Sounds simple, and it is. We will try to point out quick ways to handle these familiar circuit elements. We will concentrate on one circuit fragment, the voltage divider.

Preliminary: What is "the art of electronics?"

Not an art, perhaps, but a craft. Here's the Text's formulation of what it claims to teach:

...the laws, rules of thumb, and tricks that constitute the art of electronics as we see it. (P. 1)

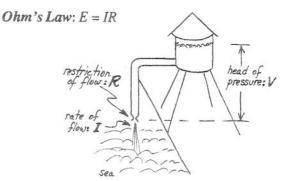
As you may have gathered, if you have looked at the text, this course differs from an engineering electronics course in concentrating on the "rules of thumb" and the "tricks." You will learn to use rules of thumb and reliable tricks without apology. With their help you will be able to leave the calculator-bound novice engineer in the dust!

#### Two Laws

Text sec. 1.01

First, a glance at two laws: Ohm's Law, and Kirchhoff's Laws (V,I).

We rely on these rules continually, in electronics. Nevertheless, we rarely will mention Kirchhoff again. We use his observations *implicitly*. We will see and use Ohm's Law a lot, in contrast (no one has gotten around to doing what's demanded by the bumper sticker one sees around MIT: *Repeal Ohm's Law!*)



E (old-fashioned term for voltage) is analog of water pressure or 'head' of water R describes the restriction of flow I is the rate of flow (volume/unit time)

Figure N1.1: Hydraulic analogy: voltage as head of water, etc. Use it if it helps your intuition

The homely hydraulic analogy works pretty well, if you don't push it too far—and if you're not too proud to use such an aid to intuition.

Ohm's is a very useful rule; but it applies only to things that behave like *resistors*. What are these? They are things that obey Ohm's Law! (Sorry folks: that's as deeply as we'll look at this question, in this course<sup>1</sup>.)

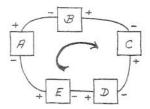
We begin almost at once to meet devices that do *not* obey Ohm's Law (see Lab 1: a lamp; a diode). Ohm's Law describes *one* possible relation between V and I in a component; but there are others.

As the text says,

Crudely speaking, the name of the game is to make and use gadgets that have interesting and useful I vs V characteristics. (P.4)

#### Kirchhoff's Laws (V,I)

These two 'laws' probably only codify what you think you know through common sense:



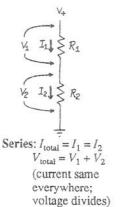
Sum of voltages around loop (circuit) is zero.

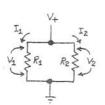


Sum of currents in & out of node is zero (algebraic sum, of course).

Figure N1.2: Kirchhoff's two laws

Applications of these laws: series and parallel circuits





Parallel:  $I_{\text{total}} = I_1 + I_2$   $V_{\text{total}} = V_1 = V_2$ (voltage same across all parts; current divides)

Figure N1.3: Applications of Kirchhoff's laws: Series and parallel circuits: a couple of truisms, probably familiar to you

Query: Incidentally, where is the "loop" that Kirchhoff's law refers to?

This is kind of boring. So, let's hurry on to less abstract circuits: to applications—and tricks. First, some labor-saving tricks.

If this remark frustrates you, see an ordinary E & M book; for example, see the good discussion of the topic in E. M. Purcell, Electricity & Magnetism, cited in the Text (2d ed., 1985), or in S. Burns & P. Bond, Principles of Electronic Circuits (1987).

Parallel Resistances: calculating equivalent R

The conductances add: conductance<sub>total</sub> = conductance<sub>1</sub> + conductance<sub>2</sub> =  $1/R_1 + 1/R_2$ 



Figure N1.4: Parallel resistors: the conductances add; unfortunately, the resistances don't

This is the easy notion to remember, but not usually convenient to apply, for one rarely speaks of conductances. The notion "resistance" is so generally used that you will sometimes want to use the formula for the effective resistance of two parallel resistors:

$$R_{\text{tot}} = R_1 R_2 / (R_1 + R_2)$$

Believe it or not, even this formula is messier than what we like to ask you to work with in this course. So we proceed immediately to some tricks that let you do most work in your head.

Text sec. 1.02

Consider some easy cases:

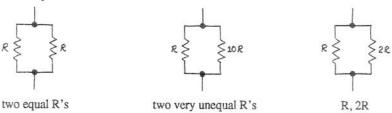
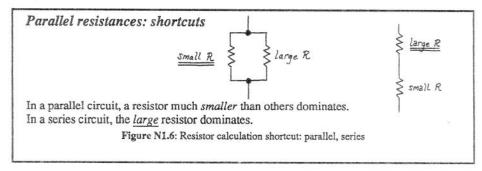


Figure N1.5: Parallel R's: Some easy cases

The first two cases are especially important, because they help one to *estimate* the effect of a circuit one can liken to either case. Labor-saving tricks that give you an estimate are not to be scorned: if you see an easy way to an estimate, you're likely to make the estimate. If you have to work to hard to get the answer, you may find yourself simply *not* making the estimate.

In this course we usually are content with answers good to 10%. So, if two parallel resistors differ by a factor of ten, then we can ignore the larger of the two.

Let's elevate this observation to a <u>rule of thumb</u> (our first). While we're at it, we can state the equivalent rule for resistors in series.



#### Voltage Divider

Text sec. 1.03

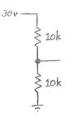


Figure N1.7: Voltage divider

At last we have reached a circuit that does something useful.

First, a note on labeling: we label the resistors "10k"; we omit " $\Omega$ ." It goes without saying. The "k" means kilo- or  $10^3$ , as you probably know.

One can calculate  $V_{\rm out}$  in several ways. We will try to push you toward the way that makes it easy to get an answer in your head.

#### Three ways:

1. Calculate the current through the series resistance; use that to calculate the voltage in the lower leg of the divider.

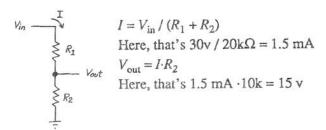


Figure N1.8: Voltage divider: first method (too hard!): calculate current explicitly

That takes too long.

2. Rely on the fact that I is constant in top and bottom, but do that implicitly. If you want an algebraic argument, you might say,

$$V_2/(V_1 + V_2) = IR_2 / (I[R_1 + R_2]) = R_2 / (R_1 + R_2)$$
 or, 
$$(1), \ V_{\text{out}} = V_{\text{in}} \ \{R_2 / (R_1 + R_2)\}$$
 In this case, that means 
$$V_{\text{out}} = V_{\text{in}} \ (10k/20k) = V_{\text{in}}/2$$

Figure N1.9: Voltage divider: second method: (a little better): current implicit

That's *much better*, and you will use formula (1) fairly often. But we would like to push you not to memorize that equation, but instead to—

3. Say to yourself in words how the divider works: something like,

Since the currents in top and bottom are equal, the voltage drops are proportional to the resistances (later, impedances—a more general notion that covers devices other than resistors).

So, in this case, where the lower R makes up half the total resistance, it also will show half the total voltage.

For another example, if the lower leg is 10 times the upper leg, it will show about 90% of the input voltage (10/11, if you're fussy, but 90%, to our usual tolerances).

#### Loading, and "output impedance"

Text sec. 1.05

Now—after you've calculated  $V_{\rm out}$  for the divider—suppose someone comes along and puts in a third resistor:

Text exercise 1.9

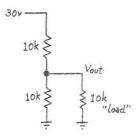


Figure N1.10: Voltage divider loaded

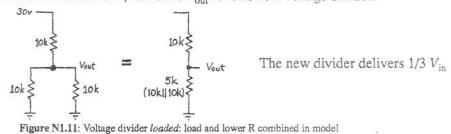
(Query: Are you entitled to be outraged? Is this no fair?) Again there is more than one way to make the new calculation—but one way is tidier than the other.

Two possible methods:

#### 1. Tedious Method:

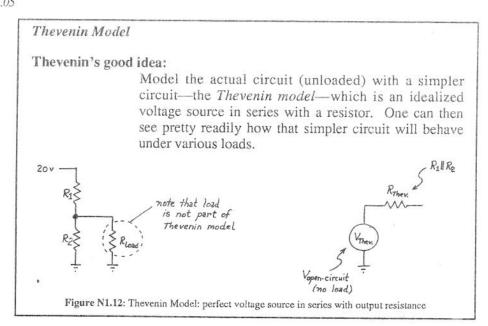
Text exercise 1.19

Model the two lower R's as one R; calculate  $V_{\rm out}$  for this new voltage divider:



That's reasonable, but it requires you to draw a new model to describe each possible loading.

# 2. Better method: Thevenin's. Text sec. 1.05



Here's how to calculate the two elements of the Thevenin model:

V<sub>Thevenin</sub>:

Just  $V_{\text{open circuit}}$ : the voltage out when nothing is attached

("no load")

R<sub>Thevenin</sub>:

Defined as the quotient of  $V_{\rm Thevenin}$  /  $I_{\rm short\text{-}circuit}$ , which is the current that flows from the circuit output to ground if you simply *short* the output to ground.

In practice, you are not likely to discover  $R_{\text{Thev}}$  by so brutal an experiment; and if you have a diagram of the circuit to look at, there is a much faster shortcut:

# Shortcut calculation of $R_{Thev}$

Given a circuit diagram, the fastest way to calculate  $R_{\mathrm{Thev}}$  is to see it as the parallel resistance of the several resistances viewed from the output.

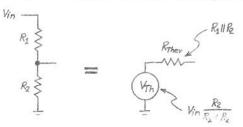


Figure N1.13:  $R_{Thev} = R_1$  parallel  $R_2$ 

(This formulation assumes that the voltage sources are ideal, incidentally; when they are not, we need to include their output resistance. For the moment, let's ignore this complication.)

You saw this result above, but this still may strike you as a little odd: why should  $R_1$ , going up to the positive supply, be treated as parallel to  $R_2$ ? Well, suppose the positive supply were set at 0 volts. Then surely the two resistances would be in parallel, right?

Or suppose a different divider (chosen to make the numbers easy): twenty volts divided by two 10k resistors. To discover the impedance at the output, do the usual experiment (one that we will speak of again and again):

A general definition and procedure to determine impedance at a point: To discover the impedance at a point: apply a  $\Delta V$ ; find  $\Delta I$ . The quotient is the impedance

This you will recognize as just a "small-signal" or "dynamic" version of Ohm's Law.

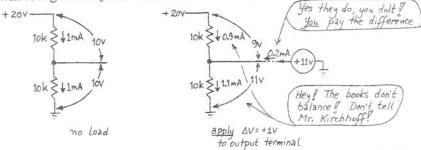


Figure N1.14: Hypothetical divider: current = 1 mA; apply a wiggle of voltage, ΔV; see what ΔI results In this case 1 mA was flowing before the wiggle. After we force the output up by 1v, the currents in top and bottom resistors no longer match: upstairs: 0.9 mA; downstairs, 1.1 mA. The difference must come from you, the wiggler.

Result: impedance =  $\Delta V$  /  $\Delta I$  = 1v / 0.2 mA = 5 k And—happily—that is the parallel resistance of the two R's. Does that argument make the result easier to accept?

You may be wondering why this model is useful. Here is one way to put the answer, though probably you will remain skeptical until you have seen the model at work in several examples: Any non-ideal voltage source "droops" when loaded. How much it droops depends on its "output impedance". The Thevenin equivalent model, with its  $R_{\rm Thevenin}$ , describes this property neatly in a single number.

# Applying the Thevenin model

First, let's make sure Thevenin had it right: let's make sure his model behaves the way the original circuit does. We found that the 10k, 10k divider from 30 volts, which put out 15v when not loaded, drooped to 10V under a 10k load. Does the model do the same?

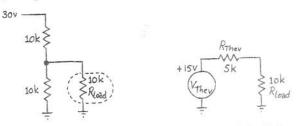


Figure N1.15: Thevenin model and load: droops as original circuit drooped

Yes, the model droops to the extent the original did: down to 10 v. What the model provides that the original circuit lacked is that single value,  $R_{\text{Thev}}$ , expressing how droopy/stiff the output is.

If someone changed the value of the load, the Thevenin model would help you to see what droop to expect; if, instead, you didn't use the model and had to put the two lower resistors in parallel again and recalculate their parallel resistance, you'd take longer to get each answer, and still you might not get a feel for the circuit's output impedance.

Let's try using the model on a set of voltage sources that differ only in  $R_{\text{Thev}}$ . At the same time we can see the effect of an instrument's input impedance.

Suppose we have a set of voltage dividers, dividing a 20v input by two. Let's assume that we use 1% resistors (value good to  $\pm 1\%$ ).

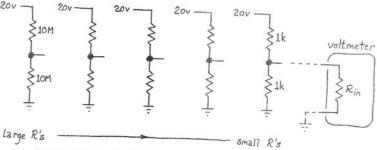


Figure N1.16: A set of similar voltage dividers: same  $V_{\mathrm{Th}}$ , differing  $R_{\mathrm{Th}}$ 's

 $V_{\rm Thev}$  is obvious, and is the same in all cases.  $R_{\rm Th}$  evidently varies from divider to divider.

Suppose now that we try to measure  $V_{\text{out}}$  at the output of each divider. If we measured with a perfect voltmeter, the answer in all cases would be 10v. (Query: is it 10.000v?)

But if we actually perform the measurement, we will encounter the  $R_{\rm in}$  of our imperfect lab voltmeters. Let's try it with a VOM ("volt-ohm-meter," the conventional name for the old-fashioned "analog" meter, which gives its answers by deflecting its needle to a degree that forms an analog to the quantity measured), and then with a DVM ("digital voltmeter," a more recent invention, which usually can measure current and resistance as well as voltage, despite its name; both types sometimes are called simply "multimeters").

Suppose you poke the several divider outputs, beginning from the right side, where the resistors are  $1k\Omega$ . Here's a table showing what we find, at three of the dividers:

| R values, divider | Measured V <sub>out</sub> 9.95 9.76 8.05 | Inference  |
|-------------------|--|--|
| 10k<br>100k       |  | within R tolerance<br>loading barely apparent<br>loading obvious |

The 8.05 v reading shows such obvious loading—and such a nice round number, if we treat it as "8 v"—that we can use this to calculate the meter's  $R_{\rm in}$  without much effort:

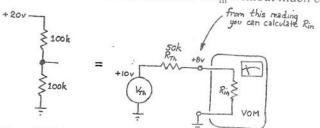


Figure N1.17: VOM reading departs from ideal; we can infer  $R_{\rm in\cdot VOM}$ 

Th gu a g As usual, one has a choice now, whether to pull out a formula and calculator, or whether to try, instead, to do the calculation "back-of-the-envelope" style. Let's try the latter method.

First, we know that  $R_{\rm Thev}$  is 100k parallel 100k: 50k. Now let's talk our way to a solution (an approximate solution: we'll treat the measured  $V_{\rm out}$  as just "8 volts":

The meter shows us 8 parts in 10; across the divider's  $R_{\text{Thev}}$  (or call it " $R_{\text{out}}$ ") we must be dropping the other 2 parts in 10. The relative sizes of the two resistances are in proportion to these two voltage drops: 8 to 2, so  $R_{\text{in-VOM}}$  must be 4 •  $R_{\text{Thev}}$ : 200k.

If we squint at the front of the VOM, we'll find a little notation, 20,000 ohms/volt

That specification means that if we used the meter on its IV scale (that is, if we set things so that an input of 1 volt would deflect the needle fully), then the meter would show an input resistance of 20k. In fact, it's showing us 200k. Does that make sense? It will when you've figured out what must be inside a VOM to allow it to change voltage ranges: a set of big series resistors. You'll understand this fully when you have done problem 1.8 in the text; for now, take our word for it: our answer, 200k, is correct when we have the meter set to the 10 V scale, as we do for this

This is probably a good time to take a quick look at what's inside a multimeter-VOM or DVM:

How a meter works:

Depends on type.

- —depends whether the basic works of the meter sense current or voltage.
- analog: senses current

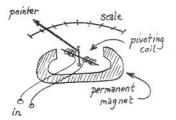


Figure N1.18: Analog meter senses current, in its guts

digital: senses voltage

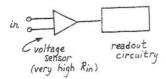


Figure N1.19: Digital meter senses voltage, in its innards

The VOM specification, 20,000 ohms/volt, describes the sensitivity of the meter movement—the guts of the instrument. This movement puts a fairly low ceiling on the VOM's input resistance at a given range setting.

Let's try the same experiment with a DVM, and let's suppose we get the following readings:

| R values, divide | Measured Vout | <u>Inference</u>   |
|------------------|---------------|--------------------|
| 100k             | 9.92          | within R tolerance |
| 1M               | 9.55          | loading apparent   |
| 10M              | 6.69          | loading obvious    |

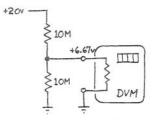


Figure N1.20: DVM reading departs from ideal; we can infer  $R_{\text{in-DVM}}$ 

Again let's use the case where the droop is obvious; again let's talk our way to an answer:

This time  $R_{\rm Th}$  is 5M; we're dropping 2/3 of the voltage across  $R_{\rm in-DVM}$ , 1/3 across  $R_{\rm Th}$ . So,  $R_{\rm in-DVM}$  must be 2• $R_{\rm Th}$ , or 10M.

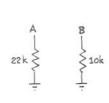
If we check the data sheet for this particular DVM we find that its  $R_{\rm in}$  is specified to be " $\geq$  10M, all ranges." Again our readings make sense.

#### VOM vs DVM: a conclusion?

Evidently, the DVM is a better voltmeter, at least in its  $R_{\rm in}$ —as well as much easier to use. As a current meter, however, it is no better than the VOM: it drops 1/4 v full scale, as the VOM does; it measures current simply by letting it flow through a small resistor; the meter then measures the voltage across that resistor.

#### Digression on ground

The concept "ground" ("earth," in Britain) sounds solid enough. It turns out to be ambiguous. Try your understanding of the term by looking at some cases:



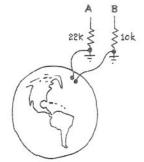


Figure N1.21: Ground in two senses

Query: what is the resistance between points A and B? (Easy, if you don't think about it too hard.) We know that the ground symbol means, in any event, that the bottom ends of the two resistors are electrically joined. Does it matter whether that point is also tied to the pretty planet we live on? It turns out that it does not.

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And where is "ground" in this circuit:

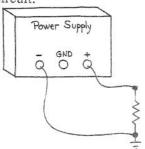


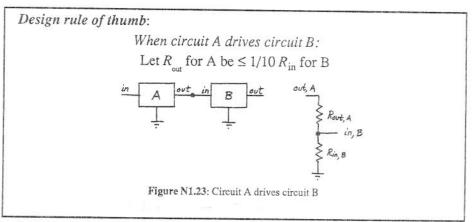
Figure N1.22: Ground in two senses, revisited

Local ground is what we care about: the common point in our circuit that we arbitrarily choose to call zero volts. Only rarely do we care whether or not that local reference is tied to a spike driven into the earth. But, be warned, sometimes you are confronted with lines that are tied to world ground—for example, the ground clip on a scope probe, and the "ground" of the breadboards that we use in the lab; then you must take care not to clip the scope ground to, say, +15 on the breadboard.

# Generalizing what we've learned of $R_{\rm in}$ and $R_{\rm out}$

The voltage dividers whose outputs we tried to measure introduced us to a problem we will see over and over again: some circuit tries to "drive" a load. To some extent, the load changes the output. We need to be able to predict and control this change. To do that, we need to understand, first, the characteristic we call  $R_{\rm in}$  (this rarely troubles anyone) and, second, the one we have called  $R_{\rm Thevenin}$  (this one takes longer to get used to). Next time, when we meet frequency-dependent circuits, we will generalize both characteristics to " $Z_{\rm in}$ " and " $Z_{\rm out}$ ."

Here we will work our way to another rule of thumb; one that will make your life as designer relatively easy. We start with a goal: *Design goal*: When circuit A drives circuit B: arrange things so that B loads A lightly enough to cause only insignificant attenuation of the signal. And this goal leads to the rule of thumb:



How does this rule get us the desired result? Look at the problem as a familiar voltage divider question. If  $R_{\text{out}A}$  is much smaller than  $R_{\text{in}B}$ , then the divider delivers nearly all of the original signal. If the relation is 1:10, then the divider delivers 10/11 of the signal: attenuation is just under 10%, and that's good enough for our purposes.

We like this arrangement not just because we like big signals. (If that were the only concern, we could always boost the output signal, simply amplifying it.) We like this

arrangement above all because it allows us to design circuit-fragments independently: we can design A, then design B, and so on. We need not consider A,B as a large single circuit. That's good: makes our work of design and analysis lots easier than it would be if we had to treat every large circuit as a unit.

An example, with numbers: What  $R_{\text{Thev}}$  for droop of < 10%? What R's, therefore?

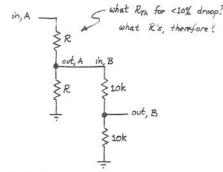


Figure N1.24: One divider driving another: a chance to apply our rule of thumb

The effects of this rule of thumb become more interesting if you extend this chain: from A and B, on to C.

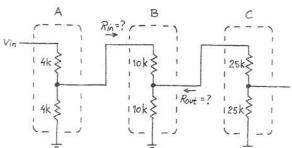


Figure N1.25: Extending the divider: testing the claim that our rule of thumb lets us consider one circuit fragment at a time

As we design C, what  $R_{\rm Thev}$  should we use for B? Is it just 10K parallel 10K? That's the answer if we can consider B by itself, using the usual simplifying assumptions: source ideal ( $R_{\rm out}=0$ ) and load ideal ( $R_{\rm in}$  infinitely large).

But should we be more precise? Should we admit that the upper branch really looks like 10K + 2K: 12k? Oh dear! That's 20% different. Is our whole scheme crumbling? Are we going to have to look all the way back to the start of the chain, in order to design the next link? Must we, in other words, consider the whole circuit at once, not just the fragment B, as we had hoped?

No. Relax. That 20% error gets diluted to half its value:  $R_{\text{Thev}}$  for B is 10k parallel 12k, but that's a shade under 5.5k. So—fumes of relief!—we need not look beyond B. We can, indeed, consider the circuit in the way we had hoped: fragment by fragment.

If this argument has not exhausted you, you might give our claim a further test by looking in the other direction: does C alter B's input resistance appreciably (>10%)? You know the answer, but confirming it would let you check your understanding of our rule of thumb and its effects.

# Chapter 1: Worked Examples: Resistors & Instruments

#### Five worked examples:

- 1. Design a voltmeter and ammeter from bare meter movement
- 2. Effects of instrument imperfections, in first lab (L1-1)
- 3. Theyenin models
- 4. R<sub>in</sub>, R<sub>out</sub>
- 5. Effect of loading

#### 1. Design a Voltmeter, Current Meter

Text sec. 1.04, ex. 1.8, p. 10

Problem: Modify a meter movement to form a voltmeter and ammeter

A 50µA meter movement has an internal resistance of 5k. What shunt resistance is needed to convert it to a 0-1 amp meter? What series resistance will convert it to a 0-10 volt meter?

This exercise gives you a useful insight into the instrument, of course, but it also will give you some practice in judging when to use approximations: how precise to make your calculations, to say this another way.

#### I amp meter

"50µA meter movement" means that the needle deflects fully when 50µA flows through the movement (a coil that deflects in the magnetic field of a permanent magnet: see Class 1 notes for a sketch). The remaining current must bypass the movement; but the current through the movement must remain proportional to the whole current.

Such a long sentence makes the design sound complicated. In fact, as probably you have seen all along, the design is extremely simple: just add a resistance in parallel with the movement (this is the "shunt" mentioned in the problem):

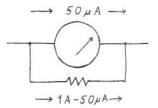


Figure X1.1: Shunt resistance allows sensitive meter movement to measure a total current of 1 A

What value?

Well, what else do we know? We know the resistance of the meter movement. That characteristic plus the full-scale current tell us the full-scale voltage drop across the movement: that's

 $V_{\mathrm{movement(full-scale)}} = I_{\mathrm{full-scale}} \circ R_{\mathrm{movement}} = 50 \; \mu\mathrm{A} \; \mathrm{\circ}5\mathrm{k}\Omega = 250 \; \mathrm{mV}$ 

Now we can choose  $R_{\text{shunt}}$ , since we know current and voltage that we want to see across the parallel combination. At this point we have a chance to work too hard, or instead to use a

sensible approximation. The occasion comes up as we try to answer the question, 'How much current should pass through the shunt?'

One possible answer is '1A less 50µA, or 0.99995 A."

Another possible answer is '1A.'

Which do you like? If you're fresh from a set of Physics courses, you may be inclined toward the first answer. If we take that, then the resistance we need is

 $R = V_{\text{full-scale}} / I_{\text{full-scale}} = 250 \text{ mV} / 0.99995 \text{A} = 0.2500125 \Omega$ 

Now in some settings that would be a good answer. In this setting, it is not. It is a very silly answer. That resistor specification claims to be good to a few parts in a million. If that were possible at all, it would be a preposterous goal in an instrument that makes a needle move so we can squint at it.

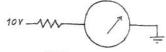
So we should have chosen the second branch at the outset: seeing that the  $50\mu A$  movement current is small relative to the the 1A total current, we should then ask ourselves, 'About how small (in fractional or percentage terms)?' The answer would be '50 parts in a million.' And that fraction is so small relative to reasonable resistor tolerances that we should conclude at once that we should neglect the  $50\mu A$ .

Neglecting the movement current, we find the shunt resistance is just  $250 mV/1A = 250 m\Omega$ . In short, the problem is very easy if we have the good sense to let it be easy. You will find this happening repeatedly in this course: if you find yourself churning through a lot of math, and especially if you are carrying lots of digits with you, you're probably overlooking an easy way to do the job. There is no sense carrying all those digits and then having to reach for a 5% resistor and 10% capacitor.

#### Voltmeter

Here we want to arrange things so that 10V applied to the circuit causes a full-scale deflection of the movement. Which way should we think of the cause of that deflection—'50µA flowing,' or '250 mV across the movement?'

Either is fine. Thinking in *voltage* terms probably helps one to see that most of the 10V must be dropped across some element we are to add, since only 0.25V will be dropped across the meter movement. That should help us sketch the solution:



← 9.75V → ← 0.25V→

Figure X1.2: Voltmeter: series resistance needed

What series resistance should we add? There are two equivalent ways to answer:

- 1. The resistance must drop 9.75 volts out of 10, when  $50\mu A$  flows; so R =  $9.75V/50\mu A = 195k\Omega$
- 2. Total resistance must be  $10V/50\mu A = 200k\Omega$ . The meter movement looks like 5k, we were told; so we need to add the difference,  $195k\Omega$ .

If you got stung on the first part of this problem, giving an answer like " $0.2500125\Omega$ ," then you might be inclined to say, 'Oh,  $50\mu A$  is very small; the meter is delicate, so I'll neglect it. I'll put in a 200k series resistor, and be just a little off.'

Well, just to keep you off-balance, we must now push you the other way: this time, " $50\mu A$ ," though a small current is not negligibly small, because it is not to be compared with some much larger current. On the contrary, it is the crucial characteristic we need to work with: it determines the value of the series resistor. And we should *not* say '200k is

close enough,' though 195k is the exact answer. The difference is 2.5%: much less than what we ordinarily worry about in this course (because we need to get used to components with 5 and 10% tolerances); but in a meter it's surely worth a few pennies extra to get a 1% resistor: a 195k.

#### 2. Lab 1-1 questions: working around imperfections of instruments

The very first lab exercise asks you to go through the chore of confirming Ohm's Law. But it also confronts you at once with the difficulty that you cannot quite do what the experiment asks you to do: measure I and V in the resistor simultaneously. Two placements of the DVM are suggested (one is drawn, the other hinted at):

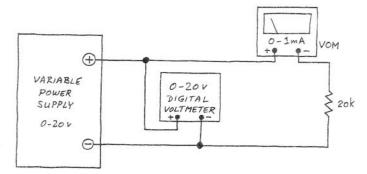


Figure X1.3: Lab 1-1 setup: DVM and VOM cannot both measure the relevant quantity

#### A Qualitative View

Just a few minutes' reflection will tell you that the voltage reading is off, in the circuit as drawn; moving the DVM solves that problem (above), but now makes the current reading inaccurate.

#### A Quantitative View

Here's the problem we want to spend a few minutes on:

#### Problem:

#### Errors caused by the Meters

If the analog meter movement is as described in the Text's problem 1.8, what percentage error in the *voltage* reading results, if the voltage probe is connected as shown in the figure for the first lab 1 experiment, when the measured resistor has the following values. Assume that you are applying 20 volts, and that you can find a meter setting that lets you get *full-scale deflection* in the current meter.

- R = 20k ohms.
- R = 200 ohms
- R = 2M ohms.

Same question, but concerning *current* measurement error, if the voltmeter probe is moved to connect directly to the top of the resistor, for the same resistor values. Assume the DVM has an input resistance of 20 M ohms.

#### Errors in Voltage readings

The first question is easier than it may appear. The error we get results from the voltage drop across the current meter; but we know what that drop is, from problem 1.8: full-scale: 0.25V. So, the resistor values do not matter. Our voltage readings always are high by a quarter volt, if we can set the current meter to give full-scale deflection. The value of the resistor being measured does *not* matter.

When the DVM reads 20V, the true voltage (at the top of the resistor) is 19.75V. Our voltage reading is high by 0.25V/19.75V—about 0.25/20 or 1 part in 80: 1.25% (If we applied a lower voltage, the voltage error would be more important, assuming we still managed to get full-scale deflection from the current meter, as we might be able to by changing ranges).

## Errors in Current readings

If we move the DVM to the top of the resistor, then the voltage reading becomes correct: we are measuring what we meant to measure. But now the current meter is reading a little high: it measures not only the resistor current but also the DVM current, which flows parallel to the current in R.

The size of *this* error depends directly on the size of R we are measuring. You don't even need a pencil and paper to calculate how large the errors are:

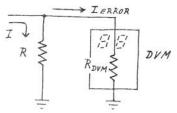


Figure X1.4: DVM causes current-reading error: how large? % error same as ratio of R to  $R_{\mathrm{DVM}}$ 

| If $R$ is $20k\Omega$ | -and the DVM looks like 20M-then one part in a   |  |
|-----------------------|--|--|
|                       | thousand of the total current flows through the DVM: the current reading will be high by 0.1%. |  |
| If R is $200\Omega$   | then the current error is minute: 1 part in 100,000: 0.001%.                                   |  |
| If R is $2M\Omega$    | then the error is large: 1 part in ten.  |  |

#### Conclusion?

There is no general answer to the question, 'Which is the better way to place the DVM in this circuit?' The answer depends on R, on the applied voltage and on the consequent ammeter range setting.

And before we leave this question, let's notice the implication of that last phrase: the error depends on the VOM range setting. Why? Well, this is our first encounter with the concept we like to call Electronic Justice, or the principle that The Greedy Will Be Punished. No doubt these names mystify you, so we'll be specific: the thought is that if you want good resolution from the VOM, you will pay a price: the meter will alter results more than if you looked for less resolution:

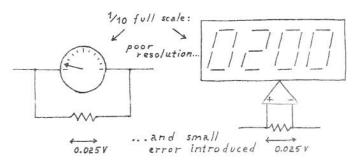
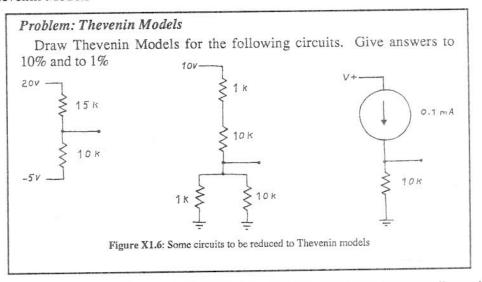


Figure X1.5: Tradeoffs, or Electronic Justice I: VOM or DVM as ammeter: the larger the reading, the larger the voltage error introduced; VOM as voltmeter: the larger the deflection at a given  $V_{\rm in}$ , the lower the input impedance

If you want the current meter needle to swing nearly all the way across the dial (giving best resolution: small changes in current cause relatively large needle movement), then you'll get nearly the full-scale 1/4-volt drop across the ammeter. The same goes for the DVM as ammeter, if you understand that 'full scale' for the DVM means filling its digital range: "3 1/2 digits," as the jargon goes: the "half digit" is a character that takes only the values zero or one. So, if you set the DVM current range so that your reading looks like

you have poor resolution: about one percent. If you are able to choose a setting that makes the same current look like 0.930, you've improved resolution 10X. But you have also increased the voltage drop across the meter by the same factor; for the DVM, like the analog VOM drops 1/4V full-scale, and proportionately less for smaller "deflection" (in the VOM) or smaller fractions of the full-scale range (for the DVM).

#### 3. Thevenin Models



Some of these examples show typical difficulties that can slow you down until you have done a lot of Thevenin models.

The leftmost circuit is most easily done by temporarily redefining *ground*. That trick puts the circuit into entirely familiar form:

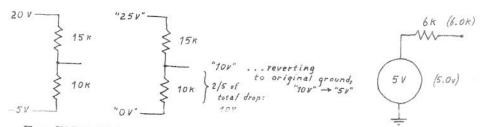


Figure X1.7: A slightly-novel problem reduced to a familiar one, by temporary redefinition of ground

The only difficulty that the middle circuit presents comes when we try to approximate. The 1% answer is easy, here. The 10% answer is tricky. If you have been paying attention to our exhortations to use 10% approximations, then you may be tempted to model each of the resistor blocks with the dominant R: the small one, in the parallel case, the big one in the

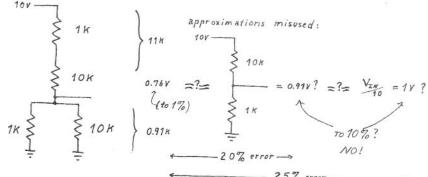


Figure X1.8: 10% approximations: errors can accumulate

Unfortunately, this is a rare case when the errors gang up on us; we are obliged to carry greater precision for the two elements that make up the divider.

This example is not meant to make you give up approximations. It makes the point that it's the *result* that should be good to the stated precision, not just the intermediate steps.

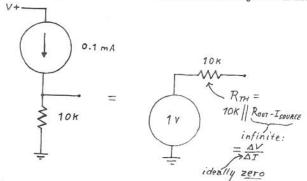


Figure X1.9: Current source feeding resistor, and equivalent Thevenin model

The current source shown here probably looks queer to you. But you needn't understand how to make one to see its effect; just take it on faith that it does what's claimed: sources (squirts) a fixed current, down toward the negative supply. The rest follows from Ohm's Law. (In Chapter 2 you will learn to design these things—and you will discover that some devices just do behave like current sources without being coaxed into it: transistors behave this way—both bipolar and FET.)

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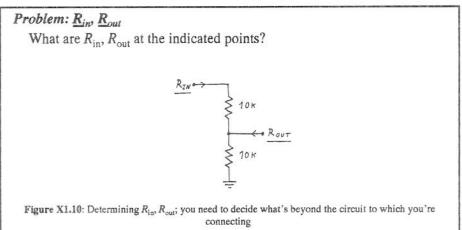
X

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The point that the current source shows a very high output impedance helps to remind us of the definition of impedance: always the same:  $\Delta V/\Delta I$ . It is better to carry that general notion with you than to memorize a truth like 'Current sources show high output impedance.' Recalling that definition of impedance, you can always figure out the current source's approximate output impedance (large versus small); soon you will know the particular result for a current source, just because you will have seen this case repeatedly.

#### 4. 'Looking through' a circuit fragment, and Rin, Rout



It's clear what  $R_{in}$  the divider should show: just  $R_1 + R_2$ : 10k + 10k = 20k. But when we say that are we answering the right question? Isn't the divider surely going to drive something down the line? If not, why was it constructed?

The answer is Yes, it is going to drive something else—the load. But that something else should show its own Rin high enough so that it does not appreciably alter the result you got when you ignored the load. If we follow our 10X rule of thumb (see the end of Class 1 notes), you won't be far off this idealization: less than 10% off. To put this concisely, you might say simply that we assume an ideal load: a load with infinite input impedance.

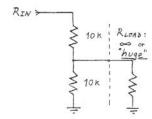


Figure X1.11:  $R_{in}$ : we need an assumption about the load that the circuit drives, if we are to determine  $R_{in}$ 

 $R_{\rm out}$ 

Here the same problem arises—and we settle it in the same way: by assuming an ideal source. The difficulty, again, is that we need to make some assumption about what is on the far side of the divider if we are to determine  $R_{\rm out}$ :

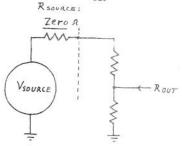
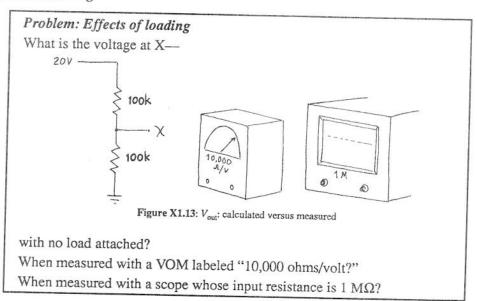


Figure X1.12:  $R_{\text{out}}$ : we need an assumption about the source that drives the circuit, if we are to determine  $R_{\text{out}}$ 

#### 4. Effects of loading



This example recapitulates a point made several times over in the the first day's class notes, as you recognize. *Reminder*: The "...ohms/volt" rating implies that on the 1-volt scale (that is, when 1V causes full deflection of the meter) the meter will present that input resistance. What resistance would the meter present when set to the 10 volt scale?

We start, as usual, by trying to reduce the circuit to familiar form. The Thevenin model does that for us. Then we add meter or scope as *load*, forming a voltage divider, and see what voltage results:

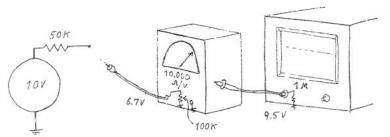


Figure X1.14: Thevenin model of the circuit under test; and showing the "load"—this time, a meter or scope

You will go through this general process again and again, in this course: reduce an unfamiliar circuit diagram to one that looks familiar. Sometimes you will do that by merely redrawing or rearranging the circuit; more often you will invoke a model, and often that model will be Thevenin's.

# Lab 1: DC Circuits

Reading: C

Chapter 1, secs 1.1 – 1.11.

Appendix A (don't worry if there are things you

don't understand)

Appendix C

Problems:

Problems in text.

Additional Exercises 1,2.

#### 1-1. Ohm's Law

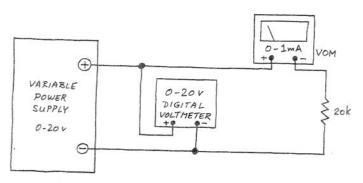


Figure L1.1: Circuit for measurement of resistor's I vs V

First, the pedestrian part of this exercise: Verify that the resistor obeys Ohm's law, by measuring V and I for a few voltages.

## A preliminary note on procedure

The principal challenge here is simply to get used to the breadboard and the way to connect instruments to it. We do not expect you to find Ohm's Law surprising. Try to build your circuit on the breadboard, not in the air. Novices often begin by suspending a resistor between the jaws of alligator clips that run to power supply and meters. Try to do better: plug the resistor into the plastic breadboard strip. Bring power supply and meters to the breadboard through jacks (banana jacks, if your breadboard has them); then plug a wire into the breadboard so as to join resistor, for example, to banana jack. Below is a sketch of the poor way and better way to build a circuit.

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your cir

Use a va L1.1. Note